REDUNDANCY

Phase Scenario	Failure / Effect Description		Criticality Hazard Reference
Failure Mode:	Fuel leaks into the closed cavity between the liner and structural jacket.	Directive #:	CCBD ME3-01-5212
Part Number:	R046300	Change #:	5
Item Number-Mode:	A335-02	Approval Date:	10/30/00
Item Name:	Large Throat Main Combustion Chamber	Approved:	M. La Croix
Volume:	Combustion Devices	Prepared:	M. Oliver

 SMC
 Leakage into the closed jacket cavity causes burst diaphragm rupture, venting the cavity into the engine fuel drain
 1

 4.1
 system. Excessive leakage causes deformation of the liner in the divergent section. Significant changes in the exhaust gases flow produces a strong shock at the downstream nozzle wall. Tube failures cause loss of fuel to the preburners and high turbine temperatures. Cavity overpressurization causes ripping of welds, sudden loss of fuel, engine failure, and aft compartment overpressurization and fire. Loss of vehicle.
 ME-B5A;

Redundancy Screen: SINGLE POINT FAIURE: N/A

DESIGN

Volume:	Combustion Devices	Prepared:	M. Oliver
Item Name:	Large Throat Main Combustion Chamber	Approved:	M. La Croix
Item Number-Mode:	A335-02	Approval Dat	e : 10/30/00
Part Number:	R046300	Change #:	5
Failure Mode:	Fuel leaks into the closed cavity between the liner and structural jacket.	Directive #:	CCBD ME3-01-5212
	Design		Document Reference
Failure Cause (s): A: Failu THE PRE-START PURGE M PASSAGES ARE DESIGNE FAILURE OF THE HOT-GA BEING LOCALLY DUMPED ESTABLISHED. USAGE LII CHAMBER HOT GAS WALL TEST. IT EXHIBITS EXCEL TEMPERATURES (2). CHA CRITICAL REGIONS OF TI OF THE SURFACE (3). ELL BECAUSE OF ITS GOOD S JACKET TO THE LINER (4 EMBRITTLEMENT PROTEC MEETS CEI REQUIREMEN REQUIREMENTS (7). THE SINCE IT CONTAINS NO F	THE IN EDNI LINER CLOSEOUL STRUCTURE CAUSED by LONG LINER INNER WALL CRACKS IN THE POSSIBILITY OF ICE FORMATION IN COOLANT PASSAGE. THE COOLAND D SUCH THAT MINOR REDUCTION IN COOLANT FLOWRATE CAN BE SUSTAINED WITH S WALL. CRACKS IN THE HOT GAS WALL GROW SLOWLY DUE TO INCREASED COOLAND THROUGH THE CRACK. USAGE LIMITS FOR MCC HOT WALL CRACKS HAVE BEEN MITS ARE DEFINED BY SPECIFICATION (1). NARLOY- Z IS USED AS THE COMBUSTION LATERIAL BECAUSE OF ITS ABILITY TO RESIST THERMAL STRAINS GENERATED DUF LLENT THERMAL CONDUCTIVITY, THERMAL FATIGUE, AND STRENGTH AT ELEVATED NNEL PASSAGES ARE DESIGNED TO ALLOW PASSAGE OF PARTICLES UP TO 0.035. THE HOT-GAS WALL ARE POLISHED TO MAINTAIN LAMINAR FLOW AND REDUCE ROUGH ECTRODEPOSITED NICKEL WAS SELECTED AS THE STRUCTURAL CLOSEOUT MATERIAL STRENGTH AND SUITABILITY IN PROVIDING A TRANSITION METAL FOR WELDING THE D.). IT HAS A BARRIER OF ELECTRODEPOSITED NICKEL (5). A PRIMARY STRESS FACTOR OF SAFE TS (6). HIGH CYCLE AND LOW CYCLE FATIGUE LIFE OF THE LINER MEETS CEI LINER PARENT MATERIALS WERE CLEARED FOR FRACTURE MECHANICS/NDE FLAW GRACTURE CRITICAL PARTS (8).	T OUT JT RING E IENING TY ROWTH	 RL00050-04, RF0001-053; 572K; R0017707; MPTR-71-175-302; SSME-72-1326; SSE-44L-03, CP320R0003B; RL00532, CP320R0003B; NASA TASK 117
Failure Cause(s): B: Jack ELECTRON BEAM BACK-U OVERPENETRATION OF E PROCESS GIVES EXCELLI SAMPLE SPECIMENS AND	et EB closeout weld overpenetration into EDNi liner. IPS PROVIDE A MINIMUM OF 50% BACKUP MATERIAL FOR PROTECTION AGAINST B CLOSEOUT WELDS INTO THE ELECTRODEPOSITED NICKEL LINER (1). THE EB WELD ENT UNIFORM WELDING WITH CONTROLLED PENETRATION. THE WELDING PROCESS I CONTROLLED PARAMETERS PER SPECIFICATION REQUIREMENTS (2).	ENTAILS	(1) R046297; (2) RA1607-071
Failure Cause(s): C: Fract THE TWO WELD JOINTS T WELD 15 (LINER TO FOR WELDABILITY AND COMP PER DRAWING REQUIREM	ture of manifold to liner welds. THAT MAY CAUSE INTERNAL LEAKAGE ARE WELD JOINT 10 (LINER TO INLET MANIFOL WARD END OF JACKET). HASTELOY "W" WAS SELECTED FOR WELD 10 DUE TO ITS ATIBILITY WITH EACH BASE METAL (1). THE WELD PREPARATION OF JOINT 10 IS SPE MENTS (2)(3). WELD JOINT 10 IS NOT SUSCEPTABLE TO HYDROGEN EMBRITTLEMENT	D) AND CIFIED DUE TO	(1) 572K; (2) R0017706; (3) R046290; (4) 572K;

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CRYOGENIC TEMPERATURES (4). WELD JOINT 15 USES NICKEL 61 FOR THE WELD MATERIAL BECAUSE OF ITS COMPATABILITY WITH INCONEL 718, THE NICKEL BASE, AND INCOLOY 903. JOINT 15 IS PRE-HEATED PRIOR TO WELDING AND IS MADE IN SEVERAL SEGMENTS TO PRECLUDE POST WELD SHRINKAGE RESULTING IN RESIDUAL STRESSES. THE WELD PREPARATION IS SPECIFIED ON THE DRAWINGS (2) (5). JOINT 15 IS PROTECTED FROM HYDROGEN EMBRITTLEMENT BY COPPER PLATING (6). THE PLATING IS CONTROLLED FOR COVERAGE AND THICKNESS BY SPECIFICATION (6). THE PRIMARY STRESS FACTORS OF SAFETY MEET CEI REQUIREMENTS (7). THE JACKET SIDE OF WELD 15 IS PROTECTED FROM HYDROGEN EMBRITTLEMENT BY AN INCOLOY 903 OVERLAY (8). RELIEF GROOVES ON BOTH SIDES OF WELD 15 REDUCE THE STRESS LEVELS IN THE WELD MATERIAL AND PREVENT DELAMINATION OF THE ELECTRODEPOSITED NICKEL (2)(8). HIGH CYCLE AND LOW CYCLE FATIGUE LIFE OF THE WELDS MEET CEI REQUIREMENTS (9). THE FMEA/CIL WELDS ARE CLEARED FOR FRACTURE MECHANICS/NDE FLAW GROWTH BY THE WELD ASSESSMENT (10). TABLE A335 LISTS ALL FMEA/CIL WELDS AND IDENTIFIES THOSE WELDS IN WHICH THE CRITICAL INITIAL FLAW SIZE IS NOT DETECTABLE AND THOSE WELDS IN WHICH THE ROOT SIDE IS NOT ACCESSIBLE FOR INSPECTION. THOSE WELDS IN WHICH THE CRITICAL INITIAL FLAW SIZE IS NOT DETECTABLE ARE ACCEPTABLE FOR FLIGHT BY RISK ASSESSMENT (10). (5) R046300;
(6) RA1109-002;
(7) RSS-8756, CP320R0003B;
(8) R046297;
(9) RL000532, CP320R0003B;
(10) RSS-8756

Failure Cause(s): All Causes

THE MCC INCORPORATES A VENT PORT TO ALLOW PASSAGE OF GASES FROM THE CLOSED LINER/JACKET AREA THROUGH THE DRAIN LINES AND OUT THE REAR OF THE VEHICLE. THE MCC BURST DIAPHRAGM VENT SYSTEM MAINTAINS A GREATER THAN 1.4 FACTOR OF SAFETY FOR START AND MAINSTAGE AND A 1.14 FACTOR OF SAFETY IS MAINTAINED FOR CUTOFF.

INSPECTION & TEST

Volume:	Combustion Devices	Prepared:	d. Early
Item Name:	Large Throat Main Combustion Chamber Approved:		T. Nguyen
Item Number-Mode:	A335-02	Approval Date	e: 10/30/00
Part Number:	R046300	Change #:	3
Failure Mode:	Fuel leaks into the closed cavity between the liner and structural jacket.	Directive #:	CCBD ME3-01-5212
Significant Characteristics	Inspection(s) / Test(s)		Document Reference
Failure Cause(s):A: FaiLINER, SLOTTED	lure in EDNi liner closeout structure caused by long liner inner wall crack	(s).	R0017706
E.D. COPPER CLOSEOUT AND	HOT WATER IMMERSION TEST CHECKS FOR PLATING DEFECTS AND ADHE	RA1609-018	
	THE ELECTRODEPOSITED COPPER AND ELECTRODEPOSITED NICKEL SPEC EXAMINED FOR CONFORMANCE PER SPECFICIATION REQUIREMENTS.	RA1609-018	
	A MASS SPEC LEAK TEST IS PERFORMED AFTER MAIN COMBUSTION CHAI PROOF TEST.	RL00874	
Failure Cause(s) B: Jac	ket FB closeout weld overnenetration into FDNi liner		
ELECTRON BEAM WELD COVER PENETRATION; R046300 WELDS 5,6,7,16,39 40	EB WELD SAMPLES MADE PRIOR TO ACTUAL WELD, VERIFY CORRECT WE AND SETUP. AN ULTRASONIC INSPECTION CHECKS THE WELD PENETRAT PROCEDURE AND PENETRATION IS CHECKED PER WELD SPECIFICATION. A MASS SPEC LEAK CHECK IS PERFORMED FOLLOWING PROOF PRESSURE	LD PENETRATION ION. THE E TEST.	RA1607-071 RA1115-001 RL00778 RA0115-116 RL00781 RL00784
WELD INTEGRITY	ALL WELDS ARE INSPECTED TO DRAWING AND SPECIFICATION REQUIREMENTS PER WELD RL10011 CLASS. INSPECTIONS INCLUDE: VISUAL, DIMENSIONAL, PENETRANT, RADIOGRAPHIC, RA1607-071 ULTRASONIC, AND FILLER MATERIAL, AS APPLICABLE. RA0115-116 RA0115-010		RL10011 RA1607-071 RA0115-116 RA0115-006 RA1115-001
	SPECIAL INSPECTIONS PER SPECIFICATIONS OF MCC CHAMBER ASSEMBL PERFORMED (INCLUDING BORING, ETCH, PENETRANT, AND WELD FILL).	Y EB WELDS ARE	RL00778 RL01129 RL00781 RL00782

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Failure Cause(s): C:	Fracture of manifold to liner welds.					
WELD INTEGRITY	ALL WELDS ARE INSPECTED TO DRAWING AND SPECIFICATION REQUIRMENT	NTS PER WELD RL10011				
	CLASS. INSPECTIONS INCLUDE: VISUAL, DIMENSIONAL, PENETRANT, RADI	OGRAPHIC, RA1607-071				
	ULTRASONIC, AND FILLER MATERIAL, AS APPLICABLE.	RA0115-116				
UNVERIFIABLE ROOT WELD	S UNVERIFIABLE ROOT WELDS ARE INSPECTED PER DRAWING AND SPECIFIC	ATION RA0115-006				
R046300 WELDS CLASS II - 10,15	REQUIREMENTS AS APPLICABLE.	RA1115-001				
	WELD 15 IS CLEANED AND VISUALLY INSPECTED USING 3X MAGNIFICATIO AFTER EACH WELD PASS. EACH WELD PASS IS PEENED FOR STRESS RELIEF	N OR GREATER R046300				
	WELD 10 ROOT PASS IS PENETRANT INSPECTED PER SPECIFICATION REQU	IREMENTS. RA0115-116				
	COMPLETED WELD JOINTS ARE LEAK TESTED PER SPECIFICATION REQUIRE	MENTS. RL00776				
	MCC ASSEMBLY IS PROOF PRESSURE TESTED PER SPECIFICATION REQUIRE	EMENTS. RL00784				
	A MASS SPEC LEAK TEST IS PERFORMED POST PROOF TEST.	RL00784				
COPPER PLATE OVERLAY ON	PLATING IS INSPECTED FOR COVERAGE AND THICKNESS PER SPECIFICATION	ON RA1109-002				
WELD 15	REQUIREMENTS.					
Failure Cause(s): Al	Causes					
ASSEMBLY INTEGRITY	THE HOT FIRE TESTING AND 2ND E & M INSPECTIONS VERIFY LINER AND W	VELD RL00050-04				
	INTEGRITY.	RL00056-06				
		RL00056-07				
	MCC HOT-GAS WALL IS INSPECTED AFTER EACH LAUNCH FOR CRACKS.	OMRSD V41BU0.029				
	A BURST DIAPHRAGM INSPECTION IS PERFORMED AFT ER HOT-FIRE FOR PC	OSSIBLE RL00050-04				
	PRESSURIZATION DUE TO LEAKAGE (LAST TEST).	RL00056-06				
		RL00056-07				
Failure History: Co	mprehensive failure history data is maintained in the Problem Reporting datab	base (PRAMS/PRACA)				
Re	Reference: NASA letter SA21/88/308 and Rocketdyne letter 88RC09761.					
Operational Use: No	at Applicable					

WELD JOINTS

Volume: I tem Name: I tem Number: Part/Alternate Number:	Combustion Devices Large Throat Main Combustion Chamber A335 R046300			Prepared: Approved: Approval Date: Change #: Directive #:			M. Oliver T. Nguyen 9/9/99 3 CCBD ME3-01-5238		
Component	Basic Part Number	Weld Number	Weld Type	Class	Root Side Not Access	Critica Flaw S Deteo HCF	l Initial ize Not table LCF	Comments	
MAIN COMBUSTION CHAMBER	R046300	5	EBW	la	х	х	х		
MAIN COMBUSTION CHAMBER	R046300	6,7	EBW	Ib	х	х	Х		
MAIN COMBUSTION CHAMBER	R046300	58,59	GTAW	П	х	х	Х		
MAIN COMBUSTION CHAMBER	R046300	10	GTAW	П	х	Х	Х		
MAIN COMBUSTION CHAMBER	R046300	11,12	GTAW	П	х	х	Х		
MAIN COMBUSTION CHAMBER	R046300	13,14	GTAW	11	Х	Х	Х		
MAIN COMBUSTION CHAMBER	R046300	15	GTAW	11	Х	Х	Х		
MAIN COMBUSTION CHAMBER	R046300	16	EBW	11	Х	Х	Х		
MAIN COMBUSTION CHAMBER	R046300	18	EBW	I	х				
MAIN COMBUSTION CHAMBER	R046300	22,23	EBW	I, Ia	Х				
MAIN COMBUSTION CHAMBER	R046300	39,40	EBW	I	Х				
MAIN COMBUSTION CHAMBER	R046300	68	GTAW	11	х	Х	х		

GTAW

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MAIN COMBUSTION CHAMBER R046300

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FIELD CONFIGURATION VARIANCES FROM CIL RATIONALE

Volume: Item Name: Item Number: Part/Alternate Number:	Combustion DevicesPrepLarge Throat Main Combustion ChamberAppiA335AppiR046300CharDire		M. Oliver T. Nguyen 10/30/00 1 CCBD ME3 -01 -5212	
Base Line Rationale	Variance	Change Rationale	Variant Dash Number	
A335-02	BURST DIAPHRAGM LEAK CHECK.	A BURST DIAPHRAGM INSPECTION IS PERFORMED AFTER HOT- NO FIRE FOR POSSIBLE LEAKAGE INTO MCC LINER CAVITY PER	DNE	
MONITOR MCC LINER CAVITY		SPECIFICATIONS (RL00050-04, RL00056-06, & RL00056-07).		
PRESSURE MEASURMENTS FOR				
EVIDENCE OF LEAKAGE (ECP		A BURST DIAPHRAGM LEAK CHECK IS PERFORMED PRIOR TO		
1343).		EACH FLIGHT PER OMRSD V41BQ0.240.		