

Component Group:

Fuel Turbopumps

CfL Item:

B200-02

Component: Parl Number; High Pressure Fuel Turbopomp RS007501

Fallure Mode:

₿ Ġ Energy loss at turbine inlet.

Prepared:

Approved:

D. Early T. Nguyen 4/21/99

Approval Date: Change #: Directive #:

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Phase	Failure / Effect Description	Criticality Hazard Reference
S 41	Loss in turbine power reduces turbopump speed, flow and discharge pressure. Decreased flow is sensed by controller which increases fluel preburner oxidizer flow. Excess turbine discharge temperature will cause redline shutdown. Mission scrub if detected by redline. Loss of vehicle due to HPFTP furbine failure may result if not detected.	1R ME-D1S.M
	Redundancy Screens: TURBOPUMP SYSTEM - SENSOR SYSTEM: UNLIKE REDUNDANCY	
	A Pass - Redundant hardware items are capable of checkoul during normal ground turnaround. B Pass - Loss of a redundant hardware items is detectable during flight. C: Pass - Loss of redundant bardware items could not result from a single credible event.	
M 41	Loss in furbine power reduces turbopump speed, flow and discharge pressure. Decreased flow is sensed by controller which increases fuel preburner exidezer flow. Excess turbine discharge temperature will cause redfine shuldown. Mission about if detected by redfine. Loss of vehicle due to HPFTP turbine failure may result if not detected.	1R ME-D1S M
	Redundancy Screens: TURBOPUMP SYSTEM - SENSOR SYSTEM; UNLIKE REDUNDANCY	
	A: Pass - Redundant hardware items are capable of checkout during normal ground turneround.	
	B: Pass - Loss of a redundant hardwere items is detectable during flight. C: Pass - Loss of redundant hardwere items could not result from a single credible event.	

## SSME FMEA/CIL DESIGN

Component Group:

Fuel Turbopumps

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B200-02

Component: Part Number: High Pressure Fuel Turbopump

Failure Mode:

RS007501

Energy loss at turbine inlet.

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D. Early T. Nguyen

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Design / Document Reference

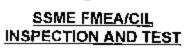
FAILURE CAUSE: A: Thermal or mechanical distortion of inlet sheet metal or thermal shield.

B: Fatigue cracking of inlet sheet metal or welds resulting in loss of pieces.

C: Thermal shield damage causing flow blockage.

ONE OF THE FUNCTIONS OF THE TURBINE BEARING SUPPORT (1) AND THERMAL SHIELD (2) IS TO DIRECT HIGH TEMPERATURE PREBURNER COMBUSTION GASES INTO THE INLET OF THE FIRST-STAGE TURBINE NOZZLE. THE THERMAL SHIELD AND WASHERS (3) ARE SUPPORTED BY AND FASTENED (4) TO THE "KAISER CAP" (5). THE THERMAL SHIELD PROTECTS THE CAP FROM DIRECT EXPOSURE TO THE HIGH VELOCITY, HIGH TEMPERATURE PREBURNER COMBUSTION GASES. TWO WASHERS (3) ARE UTILIZED TO REINFORCE THE SHIELD AT THE POINT OF THE CLAMPING FORCE FROM THE NUT (4). SEVERAL SMALLER WASHERS (3) ARE UTILIZED TO SPACE THE SHIELD TO PRECLUDE INTERFERENCE WITH THE INLET MANIFOLD (17) THE SHIELD DESIGN INCORPORATES 4 HOT-GAS VENT HOLES, WHICH REDUCES THE PRESSURE DIFFERENTIAL DURING MAINSTAGE AND PROVIDES A RAPID PRESSURE DECAY TO PRECLUDE A REVERSE PRESSURIZATION DURING TRANSIENTS. THE SHIELD AND WASHERS ARE MANUFACTURED UTILIZING HAYNES 168 (5), WHICH HAS THE REQUIRED TENSILE STRENGTH AT ELEVATED TEMPERATURES, LOW CYCLE FATIGUE, LIFE, AND RESISTANCE TO DEGRADATION AND OXIDATION IN A HIGH-PRESSURE, HYDROGEN RICH STEAM ATMOSPHERE. THE MATERIAL IS ANNEALED TO IMPROVE MECHANICAL PROPERTIES. TURBINE BEARING SUPPORT STRUCTURAL SURFACES. WHICH WOULD BE EXPOSED TO THE HIGH VELOCITY, HIGH TEMPERATURE PREBURNER GAS, ARE PROTECTED BY AN ELECTO-DISCHARGE MACHINED (EDM) LINER THAT FORMS THE TURBINE INLET MANIFOLD (17). THE MANIFOLD DUCTS THE HIGH VELOCITY, HIGH TEMPERATURE PREBURNER GAS INTO THE 1st STAGE OF THE TURBINE. THE LINER IS FABRICATED FROM A SINGLE FORGING, FIRST USING BOTH CONVENTIONAL AND EDM MATERIAL REMOVAL PROCESS. CHEM-MILLING IS USED TO REMOVE EDM RECAST LAYER. THE PART IS MEDIA FINISHED TO ENHANCE THE HIGH CYCLE FATIGUE LIFE AND HEAT TRANSFER CHARACTERISTICS. THE LINER IS THEN SPLIT INTO TWO DETAILS THAT ARE THEN CLAM-SHELLED AROUND THE SUPPORT STRUCTURAL SURFACES, CLOSE-OUT WELDS ARE USED TO REJOIN THE TWO DETAILS. THE EDM INLET DESIGN REPRESENTS A SIGNIFICANT IMPROVEMENT OVER EARLIER CONFIGURATIONS DUE TO THE INCREASED CROSS SECTIONAL THICKNESS OF THE LINER, INCREASED FILLET RADII OF THE STRUT CANS AND A REDUCTION IN THE NUMBER OF WELDS FROM 97 TO 15 TOTAL FOR THE SUB-ASSEMBLY. THIS LINER IS MANUFACTURED UTILIZING HAYNES 188 FOR THE SAME REASONS IT IS USED FOR THE THERMAL SHIELD. THE ANNULUS BETWEEN THE BEARING SUPPORT AND THE INLET MANIFOLD IS VENTED TO TURBINE INLET PRESSURE TO MINIMIZE THE POSSIBILITY OF DISTORTION. HIGH CYCLE FATIGUE INDUCED INLET MANIFOLD CRACKS DO OCCUR FROM THE OPERATIONAL ENVIRONMENT. THE CRACKING IS CONTROLLED PER THE REQUIREMENTS OF THE SHEET METAL INSPECTION SPECIFICATION (7) WHICH LIMITS THE CRACKING LENGTH, SPACING, AND SHAPE, TO PRECLUDE SHEET METAL PIECES FROM DISLODGING. THE CRITERIA IS BASED ON CRACK GROWTH RATES AND ENGINE TEST EXPERIENCE. A SIGNIFICANT REDUCTION IN LINER CRACKING HAS BEEN REALIZED OVER THE PREVIOUS DESIGNS. THE THERMAL SHIELD IS LIFE LIMITED BY MAJOR WAIVER (15). THE TURBINE BEARING SUPPORT IS LIFE LIMITED BY MAJOR WAIVER (16). CONTINUED USE WITH DISCREPANCIES IN THE INLET MANIFOLD RESULTING FROM OPERATION IS EVALUATED AND CONTROLLED PER THE REQUIREMENTS OF THE MAINTENANCE CONTROL DOCUMENT (10) THE BEARING CAP MEETS THE CEI HIGH AND LOW CYCLE FATIBUE LIFE (8) AND MINIMUM FACTORS OF SAFETY CEI REQUIREMENTS (9). THE SHIELD, WASHER AND SUPPORT PARENT MATERIALS WERE CLEARED FOR FRACTURE MECHANICS/NDE FLAW GROWTH SINCE THEY CONTAIN NO FRACTURE CRITICAL PARTS (11). THE FMEA/CIL WELDS ARE CLEARED FOR FRACTURE MECHANICS/NDE FLAW GROWTH BY THE WELD ASSESSMENT (12). TABLE B200 LISTS ALL FMEA/CIL WELDS AND IDENTIFIES THOSE WELDS IN WHICH THE CRITICAL INITIAL FLAW SIZE IS NOT DETECTABLE AND THOSE WELDS IN WHICH THE ROOT SIDE IS NOT ACCESSIBLE FOR INSPECTION. THOSE WELDS IN WHICH THE CRITICAL INITIAL FLAW SIZE IS NOT DETECTABLE ARE ACCEPTABLE FOR FLIGHT BY RISK ASSESSMENT (12). THE CONTROLLER SOFTWARE IS CONFIGURED TO DETECT AND RESPOND PROPERLY TO THE FAILURES IDENTIFIED AND COMMAND A SAFE ENGINE STATE (13). REUSE OF PARTS DURING OVERHAUL IS CONTROLLED BY THE REQUIREMENTS OF THE OVERHAUL SPECIFICATION (14).

(1) RS007524; (2) RS007549 (3) RS007676, MS9549; (4) R0015246, RS007566 R0015244; (5) RS007539; (6) RSS-8580-10; (7) RL00655; (8) RL00532, CP320R00038; (9) RSS-8546-16; CP320R0003B; (10) RSS-8793; (11) NASA TASK 117; (12) RSS-8756; (13) CP406R0002 PT 1 3.2 3:5.3; (14) RL0052B; (15) DAR 219B; (16) DAR 2987; (17) R035820



Component Group:

Fuel Turbopumps

CIL Item: Component: B200-02

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High Pressure Fuel Turbopump RS007501

Part Number:

Failure Mode: Energy loss at turbine inlet.

Prepared: Approved: Approval Date:

O. Early T. Nguyen 4/21/98

RA0115-116

Change #: Directive #:

CCBD ME3-01-5206

				GERD MIC2-01-2500	
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Failure Causes	Significant Characteristics	Inspection(s) / Test(s)		Document Reference	
A B, C	SHIELD WASHER SUPPORT INLET MANIFOLD			R\$007549 R\$007676 R\$007524 R035820	
	MATERIAL INTEGRITY	MATERIAL INTEGRITY IS VERIFIED PER ORAWING REQUIREMENTS.			
		INLET MANIFOLD CETAIL PARTS ARE PENETRANT INSPECTED PER SPECIFICATION REQUIREMENTS.		RA0115-116	
	HEAT TREAT	BEARING SUPPORT HEAT TREAT IS VERIFIED PER SPECIFICATION REQUIREMENTS		RA0611-020	
	WELD INTEGRITY	ALL WELDS ARE INSPECTED TO DRAWING AND SPECIFICATION REQUIREMENTS PER MICLASS. INSPECTIONS INCLUDE. VISUAL, DIMENSIONAL, PENETRANT, RADIOGRAPHIC, ULTRASONIC, AND FILLER MATERIAL, AS APPLICABLE.	VELO	RL10011 RA0607-094 RA0115-116 RA0115-006 RA1115-001 RA0115-127	
	ASSEMBLY INTEGRITY	THE THERMAL SHIELD SHIMMING IS VERIFIED PER DRAWING REQUIREMENTS		R5007501	
	НРЕТР		ŕ		
	ASSEMBLY INTEGRITY	THE PUMP SUBASSEMBLIES ARE INSPECTED DURING OVERHAUL PER SPECIFICATION RECLIREMENTS INSPECTIONS INCLUDE: VISION DIMENSIONAL DENETRANT AND		RL00528	

REQUIREMENTS, INSPECTIONS INCLUDE: VISUAL, DIMENSIONAL, PENETRANT, AND

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## SSME FMEAICIL FIELD CONFIGURATION VARIANCES FROM CIL RATIONALE

Component Group:

Fuel Turbopumps

Item Name:

High Pressure Fuel Turbonump

Hem Number: Part Number: B200 RS007501 Prepared: Approved: D. Early T. Nguyen 4/21/99

Approval Date: Change #:

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Base Line Rationale		Page:	1 of 2	
	Veriance	Change Rationale	Variani Dash Numbe	
1. B200-15 RS007502; CAUSE A. B200-24; RS007605; CAUSE A THE INNER AND OUTER BEARING RACES ARE EDDY CURRENT INSPECTED PER RL00743.	BEARING RACES RECEIVED FROM SUPPLIER SPLIT BALL BEARING INCORPORATED RECEIVED NO GENERAL EDDY CURRENT INSPECTION	GENERAL EDDY CURRENT INSPECTION OF RACES REPLACES TYPE IVC IN PENETRANT INSPECTION IN DETECTING SURFACE FLAWS USE AS IS RATIONALE:  1. RACES SUPPLIED BY SPLIT BALL BEARING INCORPORATED RECEIVED 10X VISUAL AND TYPE IVC PENETRANT INSPECTION INSTEAD OF GENERAL EDDY CURRENT INSPECTION. FLAW DETECTABILITY RELIABILITY LEVELS RETWEEN PENETRANT AND GENERAL EDDY CURRENT INSPECTIONS ARE 0.060 AND 0.057 RESPECTIVELY.	SEE DAR 2745 FOR VARIANT PART SERIAL NUMBERS.	
2. B200-13 R5007527, RS007532, CAUSE A & B. B200-26; RS007532; CAUSE B. DIFFUSER HIDDEN SURFACES ARE PENETRANT INSPECTED PER RL00343,	SOME DIFFUSERS MAY NOT RECEIVE THE POST PROOF TEST HIDDEN SURFACE IIIa PENETRANT INSPECTION	USE AS IS RATIONALE  1 IMPLEMENTATION OF HIDDEN SURFACE INSPECTION REQUIREMENT IS NOT A RESULT OF AN OBSERVED HARDWARE ANAQMALY BUT AS A RESULT OF ROCKETDYNE'S STAND DOWN.	SEE DAR 2751 FOR VARIANT PART SERIAL NUMBERS	
3 B200-14 CAUSE A, RS007568 B200-21 CAUSE B, RS007568 B200-26 CAUSE A, RS007568 WELD JOINTS RS007568 TABLE B200 HPFTP FMEA/CIL WELD JOINTS RS037568 HOUSING CURRENT CONFIGURATION IS THE ONE(1) PIECE "-1121 CAP, USING FOUR (4) WELDS AND FOUR (4) WELD NUMBERS	SCME HOUSINGS (POSSIBLY TWO) MAY HAVE BEEN FABRICATED WITH THE TWO (2) PIECE *-113" CAPS (THIS HAS AN EXTRA WELD: #13 AND THREE FXTRA WELD NUMBERS 13, 58 & 69)	TO REDUCE CONFUSION ON THE DRAWING AND ON THE MANUFACTURING FLOOR	SEE MCR 2524. SAME -113 DASH NUMBER.	
B200-02: CAUSE A, R\$607524 CAUSE B, R\$607524; CAUSE C, R\$607574	SOME TURBINE BEARING SUPPORTS (RS007524) ARE FABRICATED USING A WELDMENT OF HAYES 188 SHEET METAL INSTEAD OF THE EDM FORGING.	HIGH CYCLE FATIGUE INDUCED INLET SHEET METAL CRACKS OO OCCUR FROM THE CPERATIONAL ENVIRONMENT EXPERIENCED DURING ENGINE OPERATION. THE CRACKING IS CONTROLLED PER THE REQUIREMENTS:OF THE SHEET METAL INSPECTION SPECIFICATION (RL00655) WHICH LIMITS THE CRACKING LENGTH, SPACING, AND SHAPE, TO PRECLUDE SHEET METAL PIECES FROM DISLODGING. THE CRITERIA IS BASED ON CRACK GROWTH RATES AND ENGINE TEST EXPERIENCE. ANY CRACKS, WHICH EXCEED THE SPECIFICATION LIMITS, ARE WELD REPAIRED IRFO001-007). THE TURBINE BEARING SUPPORT WITH WELDED SHEET METAL IS LIFE LIMITED BY MAJOR WAIVER DAR 2709.	RS007524-201 AND SUBS.	

Component Group: Item Name:

Fuel Turbopumps High Pressure Fuel Turbopump B200

Item Number: Part Number:

RS007501

Prepared: Approved: Approvel Date: Change #: Oirective #:

D. Early T. Nguyen 4/21/99 2

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Base Line Rationale	Variance	Change Rationale	Variant Dash Number
5 B200-16 CAUSE A, B200-17 CAUSE A B200-18 CAUSE A, B200-19 CAUSE A, B200-22; CAUSE A.B.C.E	SOME LIFT-OFF SEAL HOUSING DRAIN LINES ARE FABRICATED USING INTERSECTING LINE DRILLED HOLES. THE HOLE THAT INTERSECTS THE OUTSIDE DIAMETER OF THE HOUSING FLANGE HAS A PLUG INSTALLED. THE PLUG IS THEN WELDED AT THE HOUSING OUTSIDE DIAMETER TO FORM A TICHT GAS SEAL	LOW CYCLE FATIGUE CRACKING HAS BEEN OBSERVED IN THE PLUG WELD, CRACK INITIATION AND PROPAGATION OCCURS AT SHUTDOWNCOOLDOWN ALL UNITS RECEIVE A STANDARD POST FLIGHT INSPECTIONS BY LEAK CHECK. LEAK CHECK POST FLIGHT WILL DETECT A CRACK PRIOR TO REFUGHT. POST LEAKAGE AT THE DRAIN LINE IS LIMITED TO 10 SCIM. ALL FLIGHT UNITS WILL CONTINUE TO RECEIVE A LEAK CHECK POST FLIGHT FOR THE DRAIN LINE PLUG WELD UNITL THE ENTIRE FLEET IS RETROFIT WITH THE EDM DRAIN LINE CONFIGURATION	R001923D-071 AND SUBS.

## SSME FMEA/CIL WELD JOINTS

Companent Group:

Fuel Turbopumps

CIL Item:

Component: Parl Number: High Pressure Fuel Turbopump RS007501

Prepared: Approved: D. Early T. Nguyen 4/21/99

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_					Root Side Not	Flaw 5	at Initial Size Not eclable	_	
Соттролея)	Basic Part Number	Weld Numbe	r Weld Type	Class	Access	HCF	LCF		Comments
SIIIELO	R00†2171	1-24, 29-52	GTAW	ti	×				
SHIELD	R0012171	26	GTAW	li					
LIFT-OFF SEAL	R0019230	1, 2	GTAW	JI .	×				
SHIELD	R0019788	25, 28	GTAW	I <b>i</b>					
SHIELD	R0019788	27 50	GTAW	Ц	×				
SHIELD	R0019788	51, 52	GTAW	1					
SHIFLO	R0019798	53, 55	GTAW	q					
BELLOWS	RS007505	1-4	<b>GTAW</b>	j		х			
BELLOWS	RS007505	5, 6	E <b>S</b> W	I		x			
NLET	RS007512	4	GTAW	Ī		x			
NLET	R\$007512	5-6	GTAW	1					
NLET	R\$007512	7-10, 12, 13	GTAW	1					
NLET	R\$007512	11	EBW	li .					
NLET	RS007512	14 15	GTAW	1					
NLET	RS007512	16	GTAW	i		х			
FARING SUPPORT	R\$007524	14	EBW	i					
EARING SUPPORT	RS007524	18	EBW	1	×				
EARING SUPPORT	RS007524	29, 30	GTAW	1	×	х			•
EARING SUPPORT	RS007524	1*8	GTAW	ſ	X	^			
EAR/NG SUPPORT	R\$007524	119, 121	W93	i	~				
EARING SUPPORT	RS007524	120	GTAW	II	×				
FARING SUPPORT	RS007524	229-241	GTAW	11	x				
OUSING	RS007568	75 223, 228 230 298	GTAW	ï	x	x	x		) 1 3 ;
DUSING	RS007568	14	GTAW	1					
DUSING	RS007568	48	EBW	i	×	x	U		
OUSING	RS0075EB	49	GTAW	i	×	^	×		
CUSING	R\$007565	51	GTAW	i	x	х			
DUSING	RS097568	52	GTAW	0	×	^			
DUSING					^				
OUSING	P.\$007568	53	EBW	Ī					