

Subsystem: HPOTP B500 - 4750000-700	Functional Assy: Drive Turbine Section B50002	Critical Item List Prepared by: M.T. Spencer Approved by: R.L. Pugh CIL Item: 0204	Page: 53 Issue Date: December 23, 1993 Rev. Date: December 08, 1995
CIL Item Code: 0204	FMEA Item Code: 0204	Analyst: M.T. Spencer Approved by: R.L. Pugh Rev. No.: Rev. Date: December 08, 1995 Effectivity: Hazard Ref.: See Listings Below	
Function: Drive Pump	System/Subsystem: HPOTP B500 - 4750000-700		

Operating Phase	Failure Mode, Description and Effect	Criticality
<u>Operating Phase:</u> a,m,c	<u>Failure Mode:</u> Loss of torque carrying capability. <u>Failure Cause(s):</u> A. In 90 Fracture of disk/shaft thru the splines, cooling holes, blade attachment, or loaded shoulder, due to vibration, thermal growth, material/mfg defect, overspeed, rub, or loss of cooling. B. In 18, & 19 Fracture of the splines of the left or right inducer blades, due to vibration, hub, thermal growth, FOD, material/mfg defect, or contamination C. In 17 Fracture of the splines of the main impeller blades, due to vibration, rub, thermal growth, FOD, material/mfg defect, or contamination D. In 28 Fracture of the splines of the pre-burner impeller due to vibration, rub, thermal growth, material/mfg defect, or contamination. <u>Failure Effect:</u> Loss of disk load causing over speed, burst, and case penetration with fire, and explosion. <u>System:</u> Uncontained engine damage <u>Mission/Vehicle:</u> Loss of vehicle <u>Redundancy Screens:</u> Does not apply since it is a single point failure	<u>Criticality:</u> 1 <u>Hazard Ref:</u> A) C1S/A/M/C (AT) 1A1.1.7.2.1.1, 1A1.1.7.2.3, 1A1.2.1, 1A1.2.4 1A1.2.5, 1A1.2.6, 1A1.2.7.1, 1A1.2.7.2 B) C1S/A/M/C (AT) 1A1.1.7.2.1.1, 1A1.1.7.2.3 C) C1S/A/M/C (AT) 1A1.1.7.2.1.1, 1A1.1.7.2.3 D) C1S/A/M/C (AT) 1A1.1.7.2.1.1, 1A1.1.7.2.3

B - 487

Subsystem: HPOTP B500 - 4750000-700	Critical Item List Prepared by: M.T. Spencer Approved by: R.L. Pugh CIL Item: 0204	Page: 54 Issue Date: December 23, 1993 Rev. Date: December 05, 1995
Part Name/No.	Design Considerations	Document Ref

Mn 80 Disk/shaft	<p>FAILURE CAUSE A. The design features an integral disk and shaft with slots for blade retention. Torque is transmitted through four sets of standard ANSI splines that have been sized to limit bearing stresses. Axial retention for the impeller and inducer stack is provided by a nut threaded to the shaft. The pre burner impeller is retained by a bolt threaded to the I.O. of the shaft, and located axially with a classified spacer (In 228). Bearing and stack locating shoulders on the shaft are provided with undercuts and generous fillets to minimize stress concentrations. The blade attachment zero-broach-angle reduces disk attachment stress concentrations, and with the common 3-blade slot, reduces manufacturing complexity.</p> <p>The shaft includes the roller bearing bore diameter, piloting diameters for all the rotating parts, the splines which drive the Inducers and Impeller, and the supply and return holes for the bore tube coolant.</p> <p>During operation, the main stack is subjected to speed, temperature, and pressure effects which result in increased compression of the stack elements and reduced tension in the shaft.</p> <p>The shaft is made of PWA-SP 1074 (GATORIZED IN 100), a High-elastic-modulus material which reduces radial disk deflections caused by blade loads, provides critical speed margin by resisting bending due to unbalanced loads, and offers superior strength and low cycle fatigue life while being reasonably resistant to hydrogen embrittlement.</p> <p>The disk is balanced by material removal. Two large diameter rings are provided on the disk, and multiple O.D. surfaces on the shaft for material removed.</p> <p>This part meets CEI requirements.</p> <p>DVS 4.1.2.8 which requires structural design analysis of the shaft was completed in 5/90, and can be found in FR-20729-08, and FR-20730-10.</p> <p>DVS 4.1.4.1.7.1 Strain gaged load test of the tie bolt had been completed in 1/91, and can be found in FR-20729-35,</p> <p>DVS 4.1.4.1.7.2 Turbine spin test evaluation had been completed in 12/90, and can be found in FR-20729-08 & 36.</p> <p>DVS 4.1.4.1.7.3 Turbine disk burst test to 122% of design rotor speed had been completed in 1/91, and can be found in FR-20729-38.</p> <p>DVS 4.1.4.1.7.4 Turbine disk vibration test to verify margin greater than 10% had been completed 12/89, and can be found in FR-20730-24.</p> <p>FAILURE CAUSE B. The Inducers boost inlet pressure to the impeller. Four bladed pump stages receive flow from the low pressure pump, and raise the pressure for delivery to the main impeller.</p> <p>Standard ANSI splines mate with the shaft for torque transfer. Piloting is provided by dual concentric snap.</p> <p>Development testing had resulted in several design changes to the inducers which include increasing the radial clearances to reduce dynamic forcing functions, change of the blade incidence angle to reduce cavitation, and change of blade shape to increase static and dynamic structural margin.</p> <p>Material is PWA-SP 1146 (Inconel 710) which was selected for its strength and LOX compatibility</p> <p>DVS testing number 4.1.4.1.4.1 thru .3 require spin(FR-20729-29), burst (FR-20729-43), and resonance testing (FR-20730-</p>	
Mn 18 & 19 Inducers		

DD
- 468

Subsystem: HPOTP B500 - 4760000-700
Functional Assay: Drive Turbine Section B50002

Critical Item List
Prepared by: M.T. Spencer
Approved by: R.L. Pugh
CIL Item: 0204

Page: 55
Issue Date: December 23, 1993
Rev. Date: December 08, 1995

15) have all been completed.

DVS Item 4.1.2.9 for structural design analysis has been completed, and can be found in FR-20729-3, and FR-20730-3 and 4.

These parts meet CEI requirements.

These parts were manufactured with a shot peening (AMS 2430) process.

ln 17
Main Impeller

FAILURE CAUSE C. The double inlet shrouded main impeller consists of four full blades, and four partial blades on each side of the hub. The impeller raises the fluid pressure prior to discharge to a common collector.

Standard ANSI splines mate with the shaft for torque transfer. Piloting is provided by dual concentric snap.

Material is provided at both faces of the hub for detail balancing. Final assembly trim balance is provided at the O.D. shroud by the ln 024 counter weights.

Radially inside the two inlets are cylindrical surfaces which are used for radial piloting between the impeller and the two inducers. These pilots were added to increase the stiffness of the joint between the impeller and inducers in order to address rotordynamic concerns.

Material is PWA-SP 1146 (Inconel 718) which was selected for its strength and LOX compatibility.

Mission life for the main impeller is greater than 1000 cycles.

This part meets CEI requirements.

DVS 4.1.4.1.3.1 Impeller spin test evaluation is complete, and can be found in FR 20729-41.

4.1.4.3.2 Burst spin test analysis is complete, and can be found in FR 20729-42.

4.1.2.1.3.3 Vibration NASTRAN analysis is complete, and can be found in FR 20730-14.

4.1.2.10 Unbalance forced response analysis is complete, and can be found in FR 20730-27.

4.1.2.3 Bi-stable operation, analytical verification by the DTM< P&M> etc. is complete, and can be found in FR 19847-1, and FR 20723-01 & 02.

ln 29
Preburner Impeller

FAILURE CAUSE D. The shrouded Preburner impeller has four full, and four partial blades that raise the fluid pressure for delivery to the preburner.

Standard ANSI splines mate with the shaft for torque transfer. Piloting is provided by dual concentric snap.

Two radial snap keep the impeller concentric with the shaft. Two equally spaced slots in the front face allow flow to pass into the impeller bore to provide cooling flow to the pump end bell bearing.

Trim balance as required is provided by balance weights ln 298 which is made of AMS 5646.

Material is PWA-SP 1146 (Inconel 718) which was selected for its strength and LOX compatibility.

Mission life for the P/B impeller is greater than 1000 cycles.

This part meets CEI requirements.

Subsystem: HPOTP B500 - 4750000-700
Functional Assay: Drive Turbine Section B50002

Critical Item List
Prepared by: M.T. Spencer
Approved by: R.L. Pugh
CIL Item: 0204

Page: 56
Issue Date: December 23, 1993
Rev. Date: December 08, 1995

This part is manufactured using processes which are chemical milling (PWA-SP 108), and finishing ECMR (97-5).

DVS testing number 4.1.4.1.3.1 thru .3 require spin, burst, and resonance testing. As of 04/01, resonance testing (FR 20730-16), and spin and burst tests (FR 20728-38 & 40) have been completed.

DVS Item 4.1.2.8 for structural design analysis has been completed, and can be found in FR-20728-5, and FR-20730-2, and Rotor dynamics FR-20730-27.

Subsystem: HPOTP B500 - 4750000-700
Functional Assy: Drive Turbine Section B50002

Critical Item List
Prepared by: M.T. Spencer
Approved by: R.L. Pugh
CIL Item: 0204

Page: 57
Issue Date: December 23, 1993
Rev. Date: December 08, 1995

Inspection and Test

Possible Causes	Significant Characteristics	Inspection and Test	Document Ref
Failure Cause A Mn 080 Disk/shaft/sleeve	Material Integrity	Material integrity is verified per specification requirements. Shot peen per specification.	PWA-SP 1074, PWA-SP 1146 AMS 2430
INSPECTION			
	Raw Material	Sonic - disk and shaft per QAD	
	Finished Material	FPI - disk, shaft set, sleeve per QAD	SP-FPM Master
		ECI - disk & shaft set, and detail, per QAD	SP-ECM Master
		Shaft journal diameters are verified per drawing requirements. Profile of broach slot center line is verified per drawing requirements. Spline data requirements are verified per drawing requirements.	
	Assembly Integrity	Part seating will be verified per the assembly drawing. Cleanliness of components will be verified per specification.	REI 013 PWA-SP 80
Failure Cause B Mn 018 & 019 Inducers	Material Integrity	Material integrity is verified per specification . Shot peening verified per specification.	PWA-SP 1146 AMS 2430
INSPECTION			
	Raw Material	Sonic per QAD	
	Finished Material	FPI (before balance) per QAD FPI per QAD Spline requirements verified per drawing requirements.	SP-FPM Master SP-FPM Master
		ECI per QAD	SP-ECM Master
	Assembly Integrity	Part seating will be verified per assembly drawing. Rotor assembly torque will be stretched, torqued, and locked per assembly drawing. Vibration controlled by assembly balance. Cleanliness of components will be verified per specification.	REI 013 PWA-SP 80
Failure Causes C Mn 017	Material Integrity	Material integrity is verified per specification requirements.	PWA-SP 1146

Subsystem: HPOTP 6500 - 4750000-700
Functional Assay: Drive Turbine Section B50002

Critical Item List
Prepared by: M.T. Spencer
Approved by: R.L. Pugh
CIL Item: 0204

Page: 58
Issue Date: December 23, 1993
Rev. Date: December 08, 1995

Failure Cause C
In 017
Impeller

Material Integrity

Material integrity is verified per specification requirements.

PWA-SP 1146

INSPECTION

Raw Material

Sonic per QAD

Finished Material

ECI per QAD

SP-ECM Master

Spline requirements verified per drawing requirements.

FPI per QAD

SP-FPM Master

Assembly Integrity

Part seating will be verified per assembly drawing.
Cleanliness of components will be verified per specification.

REI 013
PWA-SP 80

Vibration verified per assembly drawing.
Balance weights are staked per print requirements.

REI 003
PWA-SP 361

Failure Cause D
In 029
P/B Impeller

Material Integrity

Material integrity is verified per specification requirements.

PWA-SP 1146

ECM & ECMR

PWA-SP 108, & 87-5

Contamination control

PWA-SP 36108-4

INSPECTION

Impeller O.D. PEBB seating diameter is verified per drawing requirements.

Raw Material

Sonic- detail level per QAD

Finished Material

FPI - assembly level per QAD

SP-FPM Master

FPI - detail level per QAD

SP-FPM Master

ECI - detail level per QAD

SP-ECM Master

Assembly Integrity

Vibration verified per assembly drawing.
Balance weights are staked per print requirements.
FPI balance weights per QAD

REI 003
PWA-SP 361
SP-FPM Master

Part seating will be verified per assembly drawing.

Assy Spec PWA-SP REI 013

Tiebolt installed, torqued and locked, per the assembly drawing.
Cleanliness of components will be verified per specification.

Assy Spec PWA-SP REI 013
PWA-SP 80

Subsystem:	HPOTP B500 - 4750000-700	Critical Item List	Page:	59
Functional Assay:	Drive Turbine Section B50002	Prepared by: M.T. Spencer	Issue Date:	December 23, 1993
		Approved by: R.L. Pugh	Rev. Date:	December 08, 1995
		CIL Item: 0204		

All Causes	General Quality Requirements:	Supplier Quality Assurance requirements are included in PW-QA-6076, and include such requirements as first piece layouts. This requires the documentation of dimensions on all characteristics represented on the delivered article.	PWA-SP 300
		Inspection Methods Sheets for use in the inspection of purchased parts and assemblies contain the necessary information to insure that the requirements of the QADs, engineering drawings, and referenced documents are satisfied. For shop fabricated parts, the sheets are audited by Inspection Methods.	
		The purchase orders for vendor supplied parts must comply with PWA-SP 300, 'Control of Materials Processes and Parts', which requires the vendor to provide material, process, and dimensional information to the Quality Department.	
Acceptance	Acceptance test will be conducted as required by contract, to demonstrate specified performance.	DR SE-13	
Maintenance	Shaft rotation torque check is performed after engine operation, or HPOTP installation/reinstallation.	OMRSD-V41BSO.050	
Cleanliness	Cleanliness of components will be assured by compliance to Contamination Control Specification.	PWA-SP 36180-1	
Wavers	This section would contain a description of any limiting features of CIL hardware Not applicable at this time	DAR Numbers	