

Grumman Corporation

CRITICAL ITEMS LIST

GRUMMAN

ASSEMBLY NOMENCLATURE: MANIPULATOR FOOT RESTRAINT

PREPARED BY: L. HAHN & F. PERAZZO

REPORT NO: RMS-43 R-1

REVISION: A

DATE: 17 MAY 1990

FMEA REF	NAME, QTY & DRAWING REF DESIGNATION	CRT	FAILURE MODE AND CAUSE	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE
G1 A	Foot Platform Assembly (FPA) QTY (1) Draw C95-123	2/2	G1 - Latch fails to engage in notch in platform indexing mechanism due to structural failure of latch or latch spring as a result of defective material, contamination or galling	END ITEM Foot platform will rotate freely CREW INTERFACE N/A MISSION Astronaut cannot stabilize large payload; limited use of MFR CREW / VEHICLE None	A. Design In addition to considering the launch loads discussed under cases A1 and B1, the MFR has been designed to accommodate the following conditions in the deployed configurations: <ul style="list-style-type: none"> - Astronaut handling loads of one hundred pounds in any direction. - Initial response loads of MFR to RMS runaway accelerations (2.6 ft/sec/sec linear accler, on z axes and 0.5 rad/sec/sec Roll and about x axes) - RMS constrained motion load of 300 pounds ultimate, any point, any direction. - 140 pound couple by each foot to footplate assembly - 343 pound load applied to any tethered assembly. - The design minimizes orbital EVA thermal stresses by utilizing aluminum as the one basic structural material, coated with a low absorption thermal control coating per Grumman spec CSS-MFR-PS-001 Using the above load spectrum design safety margins of 1.14 for deformation and 1.40 for failure have been achieved. All springs are corrosion resistant and will be cycled a small fraction of nominal cyclic life in the 20 mission life of the MFR. Fatigue life based upon random response loads with appropriate stress concentration factors has been established using a scatter factor of 4.0 (e.g., 80 mission fatigue life based upon S-N curves). All materials are per table 1 and 2 of MSFC-SPEC-522A to reduce stress corrosion, and are certified for traceability/quality.

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CRITICAL ITEMS LIST

PREPARED BY: L. HAHN & F. PERAZZO

REPORT NO: RMS-91-R6

REVISION: R6

DATE: 6 JULY 1986

ASSEMBLY NUMBER/TYPE: MANIPULATOR FOOT RESTRAINT

ASSEMBLY PART NO: 860 304001A

FMEA REF	NAME, QTY & DRAWING REF DESIGNATION	CRIT	FAILURE MODE AND CAUSE	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE
G1 A	Foot Platform Assembly (FPA) QTY (1) Dwg C95-123	2/2	G1 - Latch fails to engage in notch in platform indicating mechanism due to structural failure of latch or latch spring as a result of defective material, contamination or galling	END ITEM Foot platform will rotate freely GEE INTERFACE N/A MISSION Astronaut cannot stabilize large payload, limited use of MFR CREW / VEHICLE None	B. TEST HISTORY 1. Acceptance test per procedure 380-34-01 at Grumman (7/7/83) before and after all tests. ATP includes functional tests of all operating functions and a general visual inspection. 2. Stability test per procedure 380-10-01 at Grumman (7/11/83). Demonstrated stanchion end play less than .6 inch for five pounds load in any direction and deflection less than 3 inches lateral and 2 inches longitudinal for 1 hundred pound loads. 3. Vibration and shock test per procedure 380-38-01 at Grumman (7/2/83). Demonstrated ability to withstand design levels without structural failure with no significant resonance. Several screens required the application of loads. 4. APC/MFR ultimate load tests per ST589 0944 at Bockwell (9/1/83). Loads applied in 10 steps, each comprising 10% of total load no yield was observed at the ultimate load of 14.5 kN. 5. Thermal vacuum test at JSC (7/25/84). MFR was operated in ambient temperature, plus 22.1 and -17.1 (average lowest achievable chamber temp) of an average vacuum of 0.0006 torr. 6. Center of gravity test at JSC (10/2/84). 7. Moment of inertia testing test at JSC (11/4/84).